High Vacuum System Engineering Calculations

2.75" Conflat High Vacuum System

Design Iteration #2

Molecular and Transitional Flow with Deuterium at 20C

CONDUCTANCE CALCULATIONS – MOLECULAR FLOW (For Use with Injected Deuterium Beam Neutron Systems @ <10^-3 Torr)

1.) Diffusion Pump

→ Max Pumping Speed of Diffusion Pump (Hydrogen)

$$\rightarrow S_{diff} = 800 \ l/sec$$

2.) Diffusion Pump to 2.75" Conflat Adapter Plate

→ Conductance of a Tube

$$C_m = 3.8(\frac{T}{M})^{\frac{1}{2}} \frac{D^3}{L}$$

 $C_m = conductance (I/sec)$

T = temperature (K) = 293.15

M = molecular mass = 2.014 (average AMU of deuterium)

D = diameter (cm) = 3.556

L = length (cm) = 2.54

 $C_m = 811.616 \ l/sec$

→ Conductance of a Short Tube

$$C_{short} = C_m (1 + \frac{4D}{3L})^{-1}$$

C_{short} = conductance of short tube (I/sec)

 C_m = conductance of a long tube (l/sec) = 811.616

D = diameter (cm) = 3.556

L = length (cm) = 2.54

 $C_{short} = 283.122 \ l/sec$

\rightarrow for L/D < 5, above equation is valid for short pipes, with error

$$L/D = 0.714$$

~+12% error max:

$$C_{shortFinal} = C_{short} \times 0.88$$

 $C_{shortFinal} = C_{short} \times 0.88$ $C_{shortFinal} = 249.147 \ l/sec$

$\rightarrow C_{adapter} = 249.147 \ l/sec$

3.) 2.75" Conflat Inline Poppet Valve

→ Conductance of a Tube

$$C_m = 3.8(\frac{T}{M})^{\frac{1}{2}}\frac{D^3}{L}$$

C_m = conductance (I/sec)

T = temperature (K) = 293.15

M = molecular mass = 2.014 (average AMU of deuterium)

D = diameter (cm) = 3.556

L = length (cm) = 4.336

 $C_m = 475.439 \ l/sec$

→ Conductance of a Short Tube

$$C_{short} = C_m (1 + \frac{4D}{3L})^{-1}$$

C_{short} = conductance of short tube (I/sec)

 C_m = conductance of a long tube (I/sec) = 475.439

D = diameter (cm) = 3.556

L = length (cm) = 4.336

 $C_{short} = 227.105 \ l/sec$

→ for L/D < 5, above equation is valid for short pipes, with error

$$L/D = 1.219$$

~+12% error max:

 $C_{shortFinal} = C_{short} \times 0.88$ $C_{shortFinal} = 199.852 \ l/sec$

→ for L/D < 5, max +8% error for equivalent length straight tube

$$L/D = 1.219$$

~+8% error max:

 $C_{shortFinal} = C_{short} \times 0.92$

 $C_{shortFinal} = 183.864 \ l/sec$

→ Total Conductance of x2 Equivalent 90 Degree Bends in Series

$$C_{poppet_valve} = \frac{c_{bend_1} \times c_{bend_2}}{c_{bend_1} + c_{bend_2}}$$

 $C_{bend_1} = C_{bend_2} = C_{ShortFinal} = 183.864 \ l/sec$

 $C_{poppet\ valve} = 91.932\ l/sec$

 $\rightarrow C_{nonnet\ valve} = 91.932\ l/sec$

4.) 2.75" Conflat Butterfly Valve

→ Conductance of a Tube

$$C_m = 3.8(\frac{T}{M})^{\frac{1}{2}}\frac{D^3}{L}$$

 $C_m = conductance (I/sec)$

T = temperature (K) = 293.15

M = molecular mass = 2.014 (average AMU of deuterium)

D = diameter (cm) = 3.556

L = length (cm) = 2.54

 $C_m = 811.616 \ l/sec$

→ Conductance of a Short Tube

$$C_{short} = C_m (1 + \frac{4D}{3L})^{-1}$$

C_{short} = conductance of short tube (I/sec)

 C_m = conductance of a long tube (I/sec) = 811.616

D = diameter (cm) = 3.556

L = length (cm) = 2.54

 $C_{short} = 283.122 \ l/sec$

→ for L/D < 5, above equation is valid for short pipes, with error

$$L/D = 0.714$$

~+12% error max:

 $C_{shortFinal} = C_{short} \times 0.88$

 $C_{shortFinal} = 249.147 \ l/sec$

→ Correction for Equivalent Cross-sectional Obstructed Area of Butterfly Valve at Max Open Position

$$Area_{short\ tube} = \pi r^2$$

r = 1.778 cm

 $Area_{short\ tube} = 9.931\ cm^2$

 $Area_{butterly\ valve\ open\ cross\ section} = \pi r^2 - L_1 W_1 - L_2 W_2$

r = 1.778 cm

 L_1 = cross-sectional length of butterfly valve shaft = 3.556 cm

 W_1 = cross-sectional width of butterfly valve shaft = 0.397 cm

 L_2 = cross-sectional length of butterfly valve in max open position from above = 3.556 cm

 W_2 = cross-sectional width of butterfly valve in max open position from above = 0.556 cm

 $Area_{butterly_valve_open_cross_section} = 6.543 cm^2$

 $Ratio_{butterfly_valve_to_unimpeded_pipe} = Area_{butterfly_valve_open_cross_section}/Area_{short_tube}$

 $Ratio_{butterfly_valve_to_unimpeded_pipe} = 0.658$

→ Corrected Conductance for Butterfly Valve at Max Open Position

 $C_{butterfly_valve} = C_{short_final} \times Ratio_{butterfly_valve_to_unimpeded_pipe}$

 $C_{butterfly_valve} = 249.147 \times 0.658$

 $C_{butterflv\ valve} = 163.939\ l/sec$

 $\rightarrow C_{butterfly_valve} = 163.939 \ l/sec$

5.) 2.75" Conflat 4-Way Cross

→ Conductance of a Tube

$$C_m = 3.8(\frac{T}{M})^{\frac{1}{2}}\frac{D^3}{L}$$

 $C_m = conductance (I/sec)$

T = temperature (K) = 293.15

M = molecular mass = 2.014 (average AMU of deuterium)

D = diameter (cm) = 3.556

L = length (cm) = 12.492

 $C_m = 165.026 \ l/sec$

→ Conductance of a Short Tube

$$C_{short} = C_m (1 + \frac{4D}{3L})^{-1}$$

 C_{short} = conductance of short tube (I/sec)

 C_m = conductance of a long tube (I/sec) = 37.054

D = diameter (cm) = 3.556

L = length (cm) = 12.492

 $C_{short} = 119.623 \ l/sec$

→ for L/D < 5, above equation is valid for short pipes, with error

$$L/D = 3.5$$

~+9% error max:

 $C_{shortFinal} = C_{short} \times 0.91$

 $C_{shortFinal} = 108.857 \ l/sec$

$\rightarrow C_{cross} = 108.857 \ l/sec$

6.) TOTAL SYSTEM CONDUCTANCE

→ Conductance of Pipeline

$$\frac{1}{c_{pipeline}} = \frac{1}{c_{adapter}} + \frac{1}{c_{poppet_valve}} + \frac{1}{c_{butterfly_valve}} + \frac{1}{c_{cross}}$$

$$\frac{1}{c_{pipeline}} = \frac{1}{249.147} + \frac{1}{91.932} + \frac{1}{163.939} + \frac{1}{108.857}$$

$$C_{pipeline} = 33.137 \ l/sec$$

$$\rightarrow C_{pipeline} = 33.137 \ l/sec$$

→ Effective Pumping Speed of the System

$$\frac{1}{S_e} = \frac{1}{C_{pipeline}} + \frac{1}{S_{diff}}$$

$$S_e = \frac{C_{pipeline} \times S_{diff}}{C_{pipeline} + S_{diff}}$$

$$C_{pipeline} = 33.137 \ l/s$$

$$S_{diff} = 800 \ l/s$$

$$S_e = 31.819 \ l/s$$

$$\rightarrow S_e = 31.819 \ l/sec$$